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Building Envelope Design by Hygrothermal Simulations

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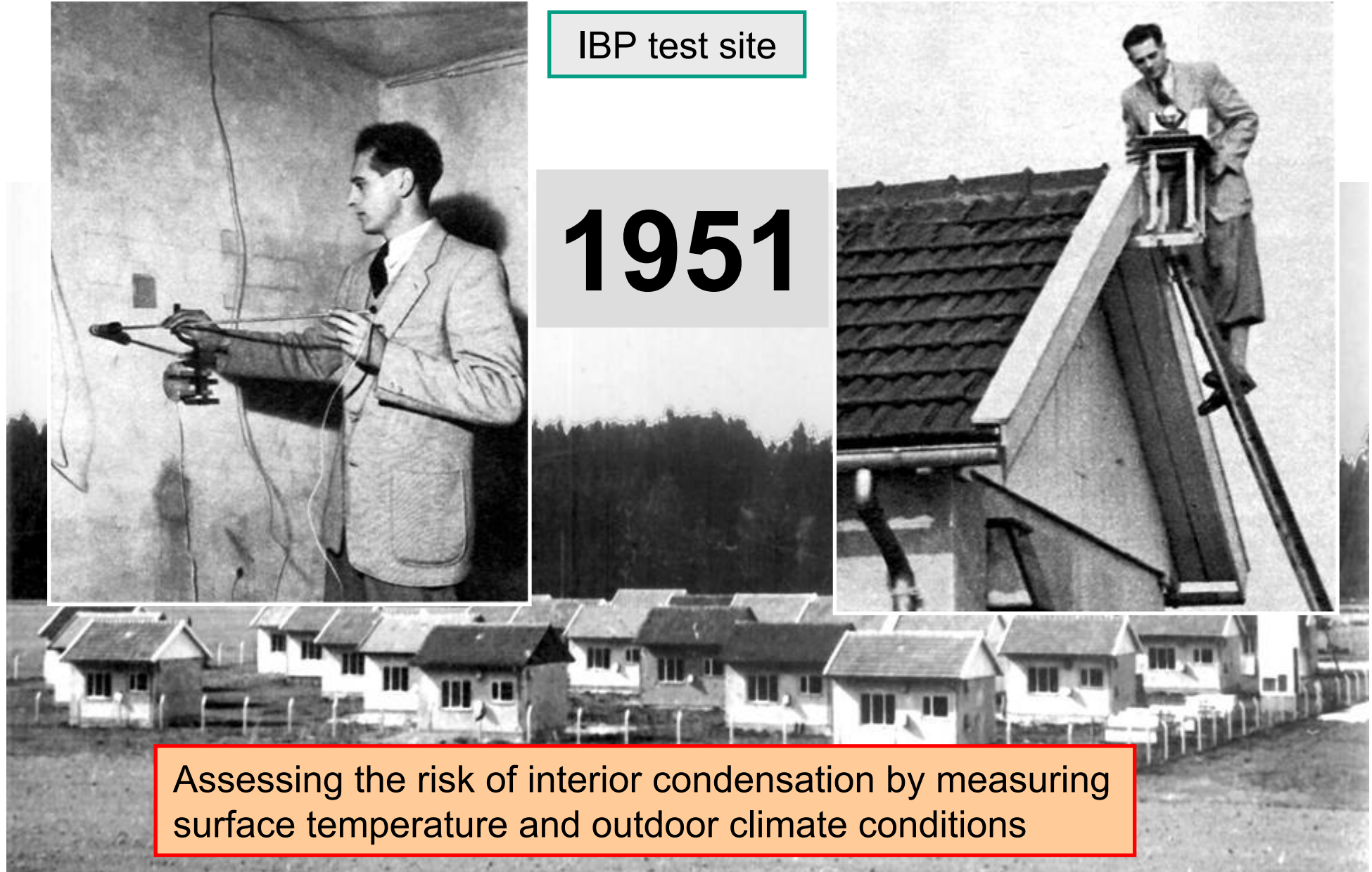
From field tests to simulations

Model fundamentals

Experimental Validation

Conclusions and Outlook

Building Envelope Design by Hygrothermal Simulations



Building Envelope Design by Hygrothermal Simulations

Steady-state Calculation

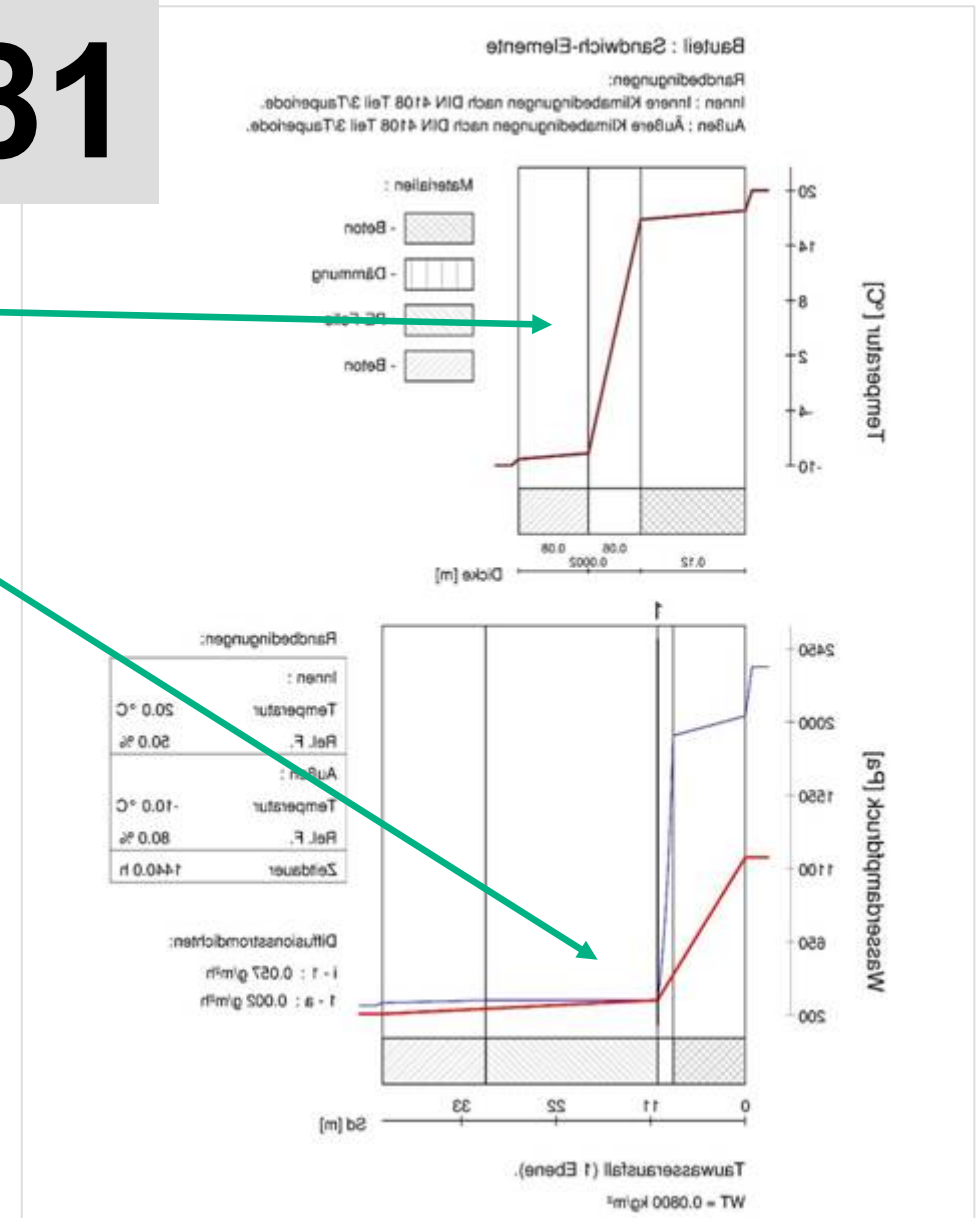
Glaser / Dew Point Method

1981

- ▶ Determine temperature gradient for steady-state condensation conditions
- ▶ Plot vapour and saturation pressure gradients over diffusion resistance of building assembly to calculate the amount of condensate

Problems

- ▶ no heat and moisture storage
- ▶ no liquid flow
- ▶ no coupling of heat and moisture transfer



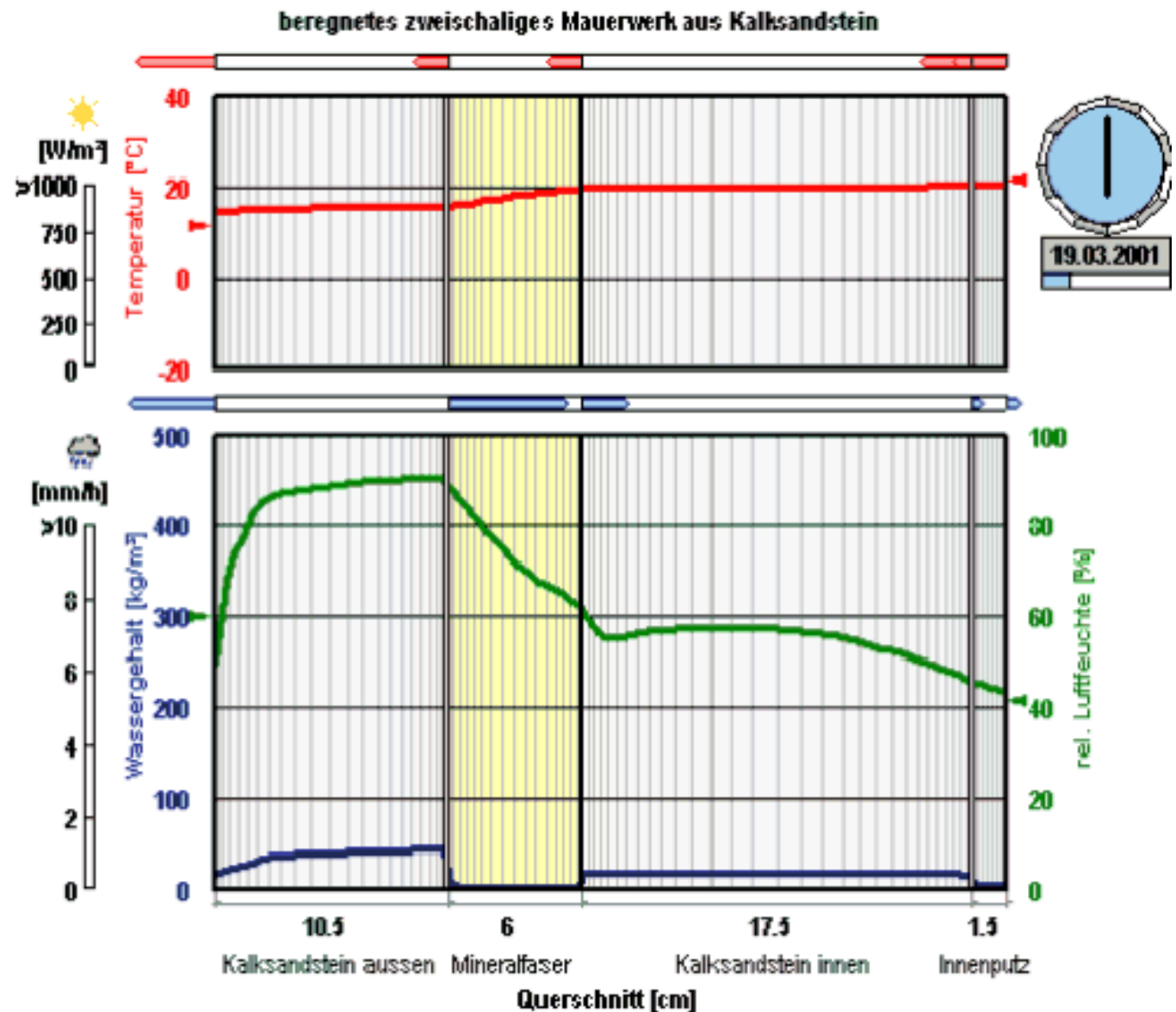
Today

Moisture control by transient simulation according to:
prEN 15026
WTA-Guideline 6-2-01
ASHRAE 160P
ASTM MNL 40

WUFI® simulation of west facing cavity wall MW insulation

Klimaort Holzkirchen

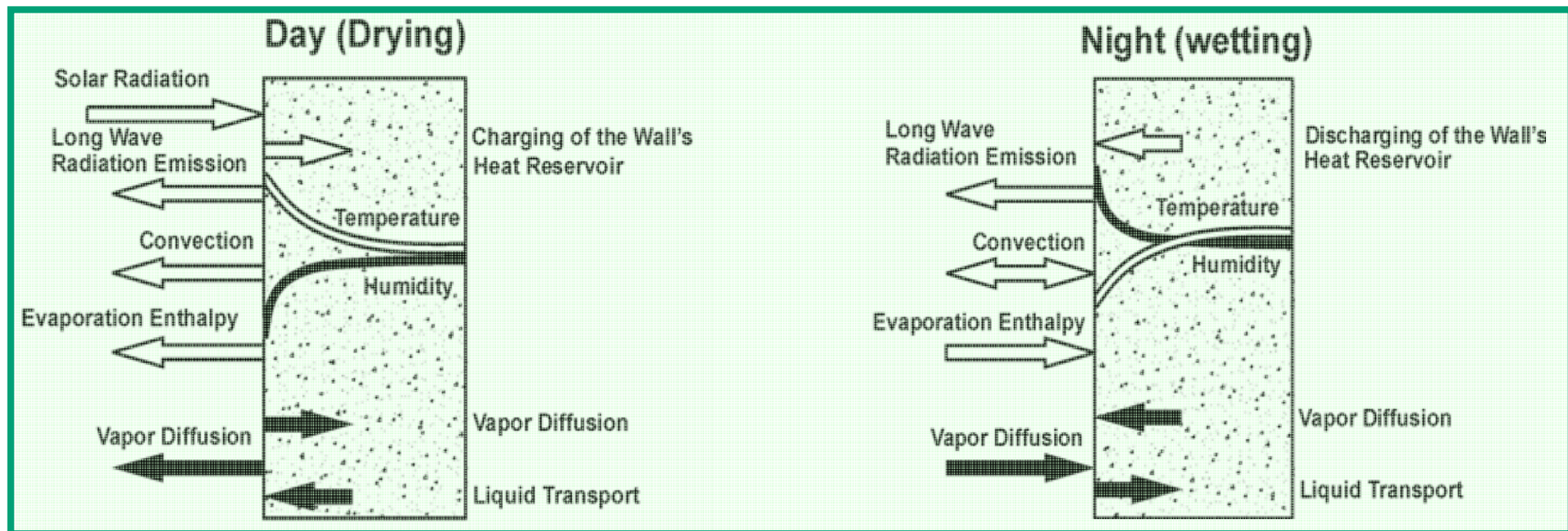
WUFI®



Model Fundamentals

In addition to steady-state diffusion models like “Glaser” hygrothermal models must include:

- ▶ heat and moisture storage
- ▶ liquid flow
- ▶ coupling of heat and moisture transfer
- ▶ effects of radiation and rain



Model Fundamentals

Heat storage

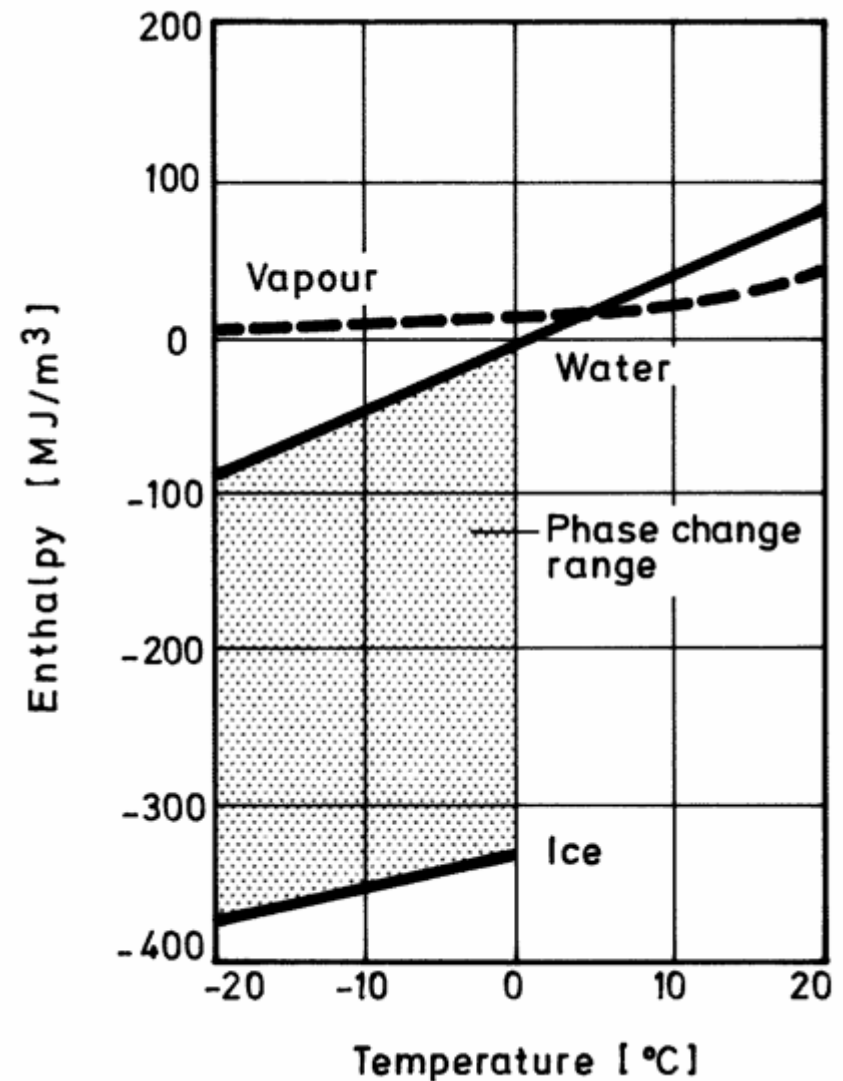
- ▶ Heat storage of dry material

$$h_d = \rho_s \cdot c_s \cdot \vartheta$$

- ▶ Heat storage wet material

$$h_m = h_d + h_{\text{water}}$$

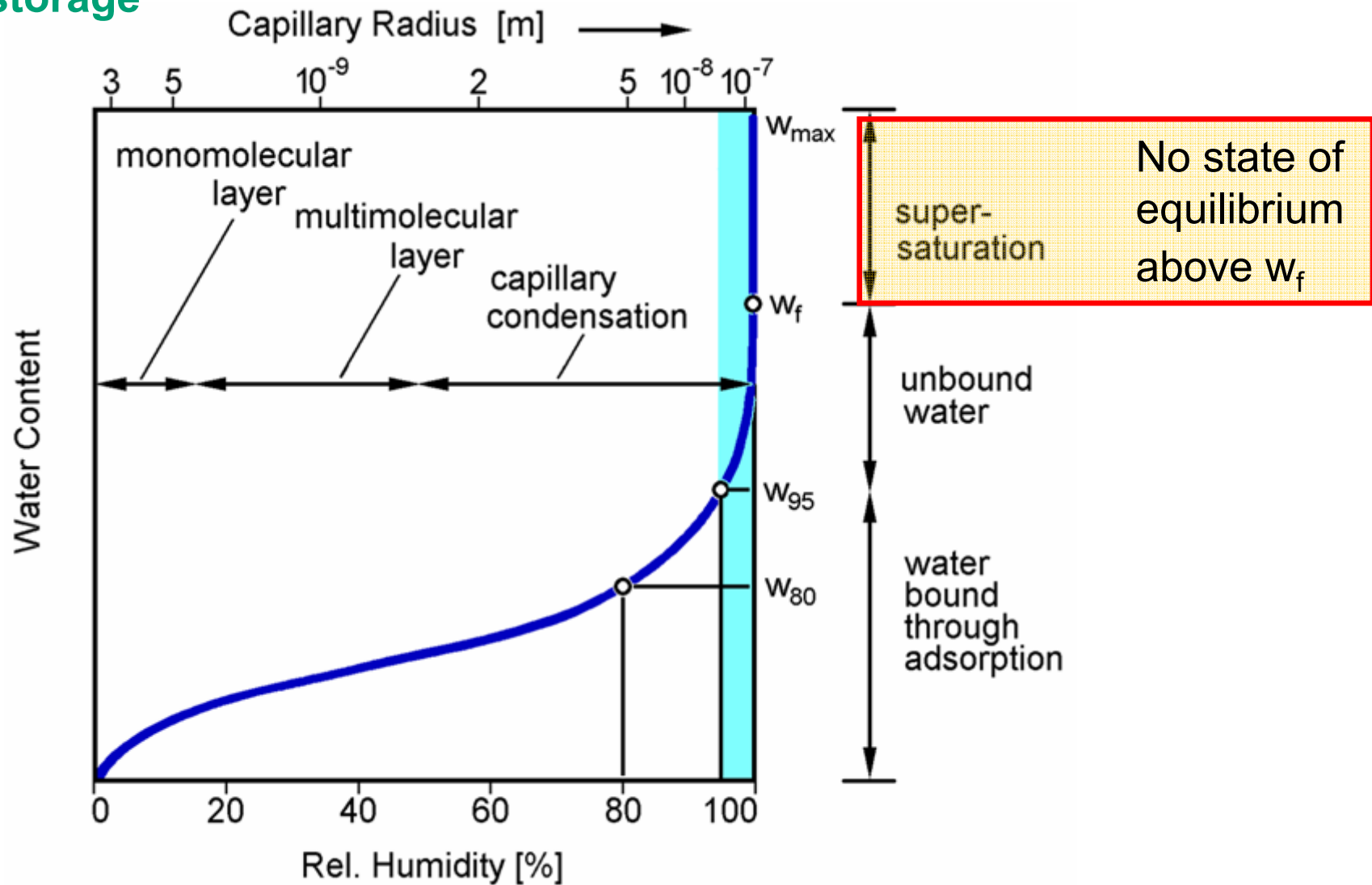
- ▶ Heat of fusion water (ice ↔ water)



Building Envelope Design by Hygrothermal Simulations

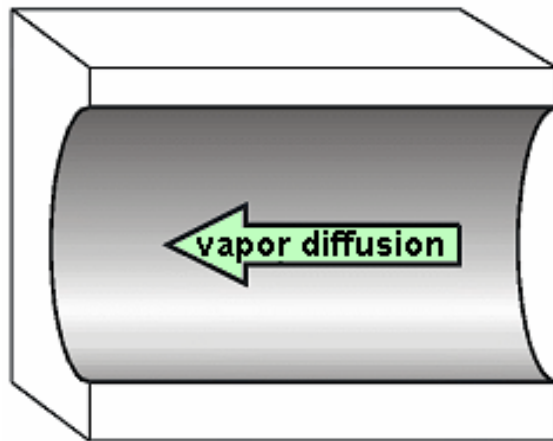
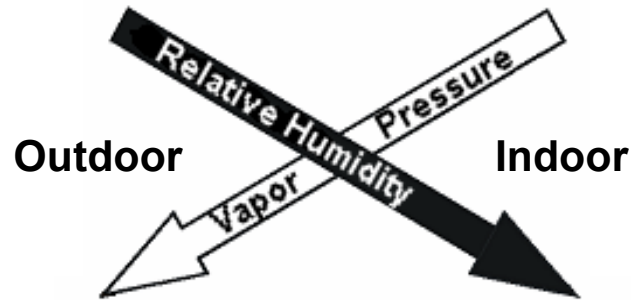
Model Fundamentals

Moisture storage



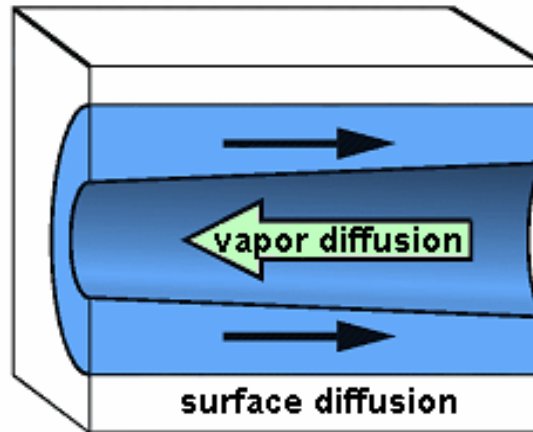
Model Fundamentals

Moisture transport (vapour and liquid)



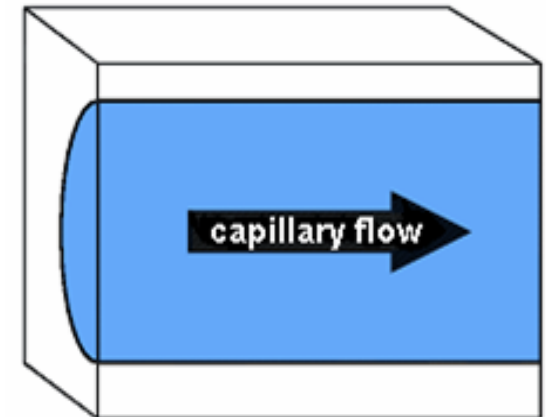
dry

$$g_v = -\frac{\delta}{\mu} \cdot \nabla p_v$$



moist

$$g_l = -D_s \cdot \nabla \varphi$$



wet

$$g_l = -D_{pc}(p_c) \cdot \nabla p_c - D_w(w) \cdot \nabla w - D_\varphi(w) \cdot \nabla \varphi$$

Model Fundamentals

Coupled transport equations

- ▶ Exponential increase of saturation pressure with temperature
- ▶ Moisture depending thermal conductivity
- ▶ Enthalpy flow by vapour diffusion with phase change

Coupled differential equations have to be solved numerically.

Heat transfer

$$\frac{\partial H}{\partial T} \cdot \frac{\partial T}{\partial t} = \nabla \cdot (\lambda \nabla T) + h_v \nabla \cdot (\delta_p \nabla (\phi p_{sat}))$$

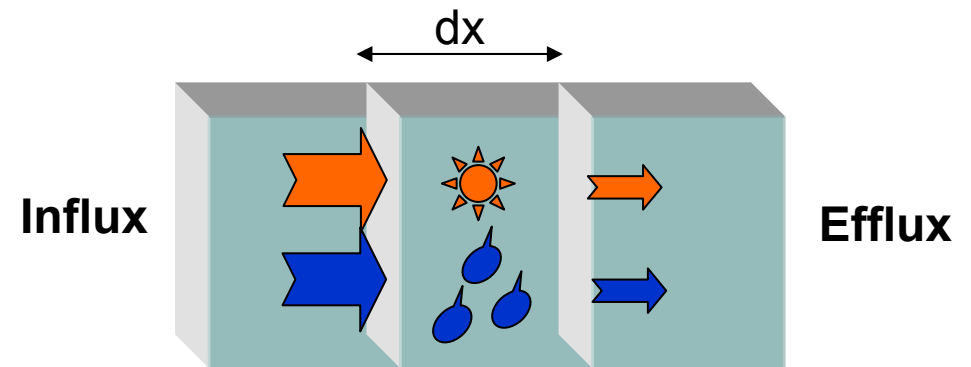
Moisture transfer

$$\frac{\partial w}{\partial \phi} \cdot \frac{\partial \phi}{\partial t} = \nabla \cdot (D_\phi \nabla \phi + \delta_p \nabla (\phi p_{sat}))$$

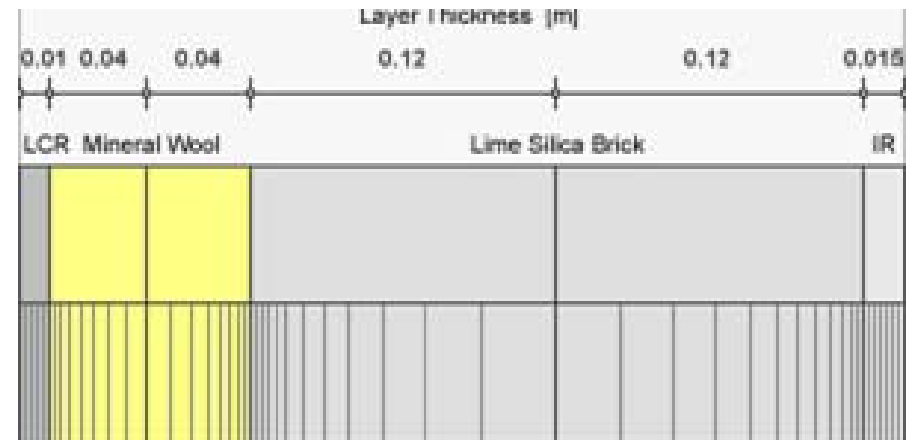
Building Envelope Design by Hygrothermal Simulations

Model Fundamentals

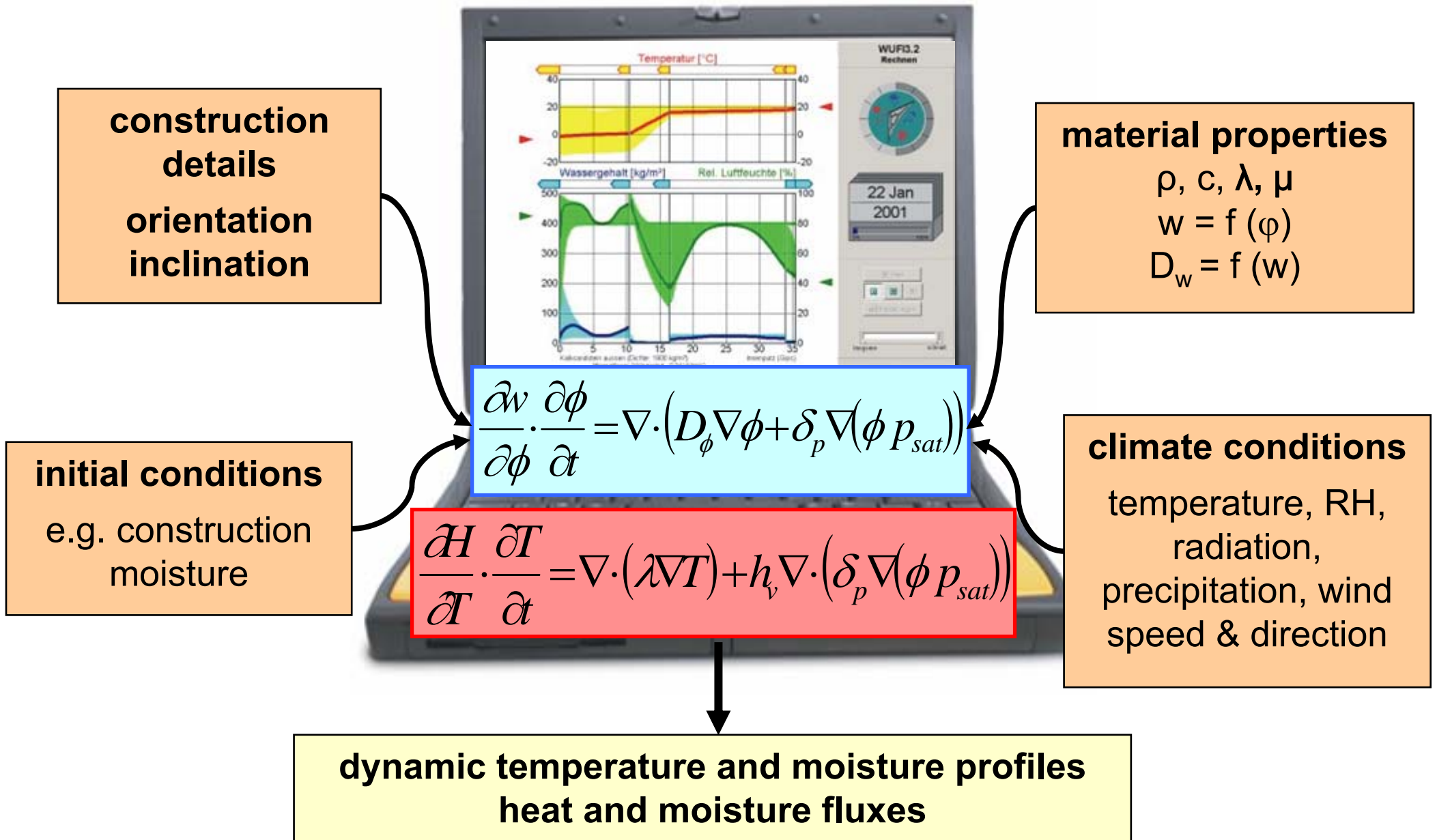
- ▶ Conservative discretisation: implicit finite volumes
- ▶ Iterative coupling by subsequent solution of transfer equations with under-relaxation
- ▶ Matrix-solver: Thomas-Algorithm (1D) or ADI (2D)



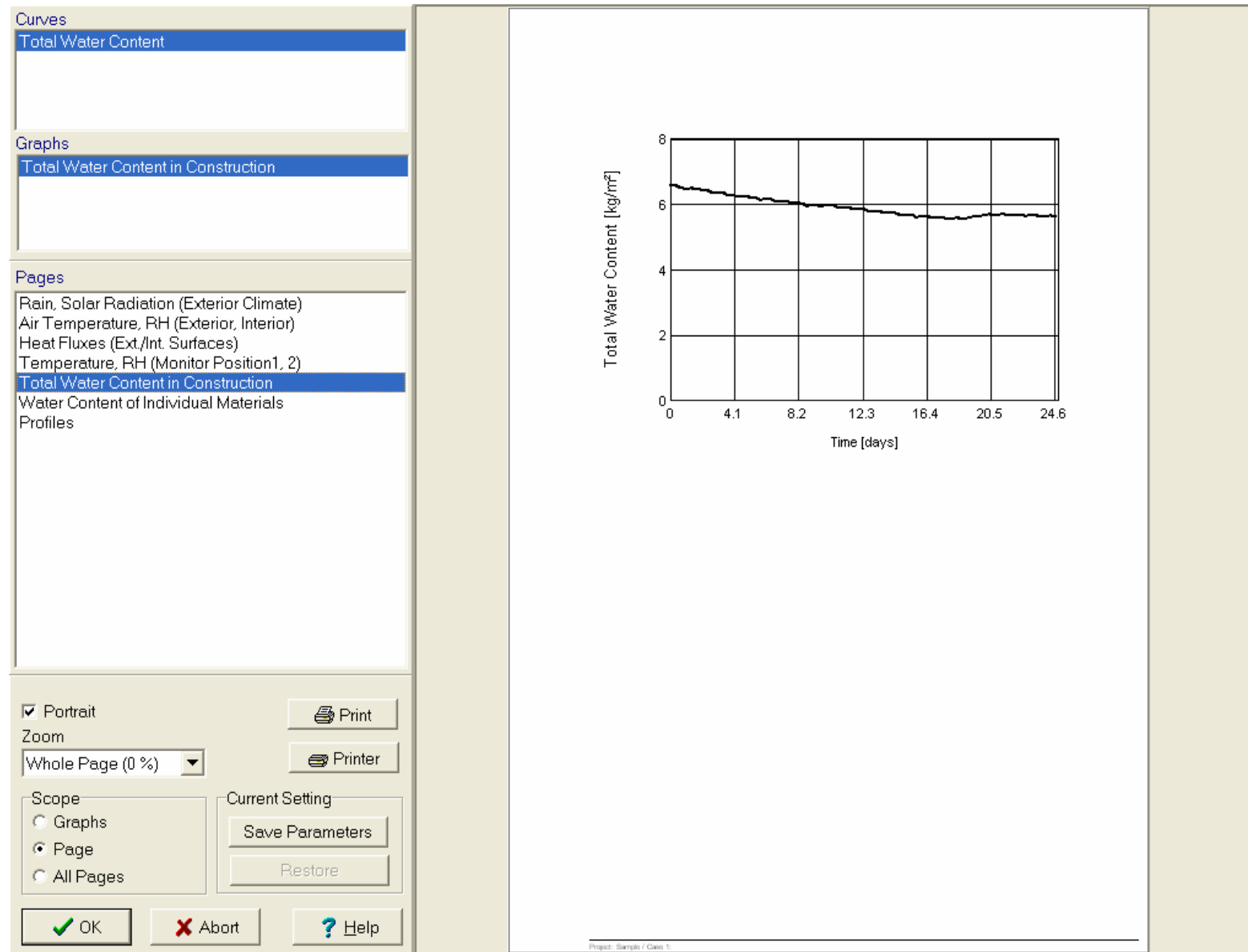
$$\frac{\partial}{\partial t} A = -\vec{\nabla} \cdot \vec{a} + \text{Sources / Sinks}$$

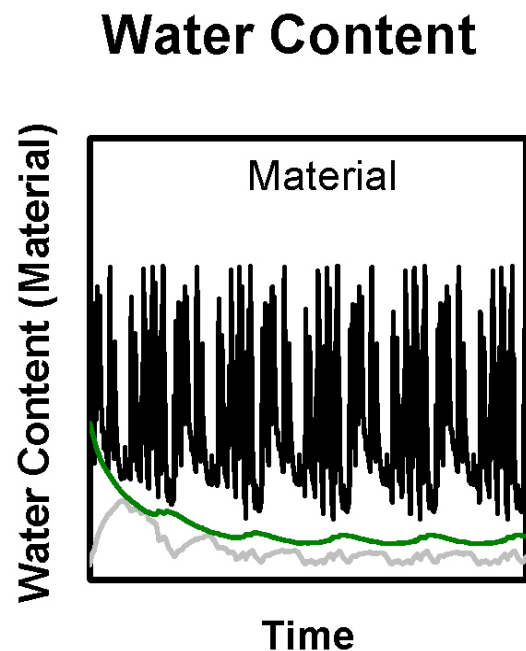
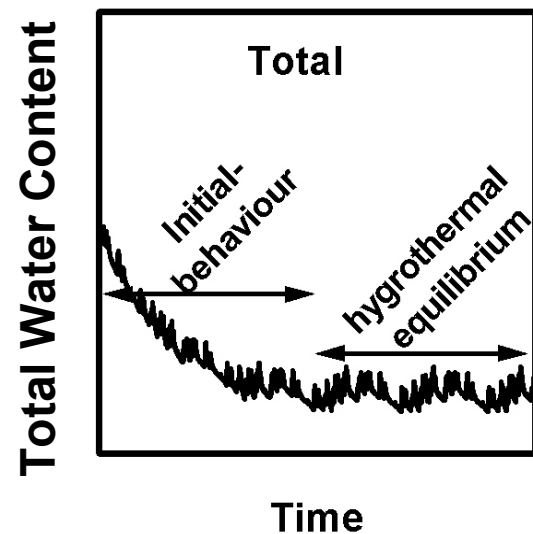


Building Envelope Design by Hygrothermal Simulations



Building Envelope Design by Hygrothermal Simulations





Performance Criteria:

$u_{\max.}$

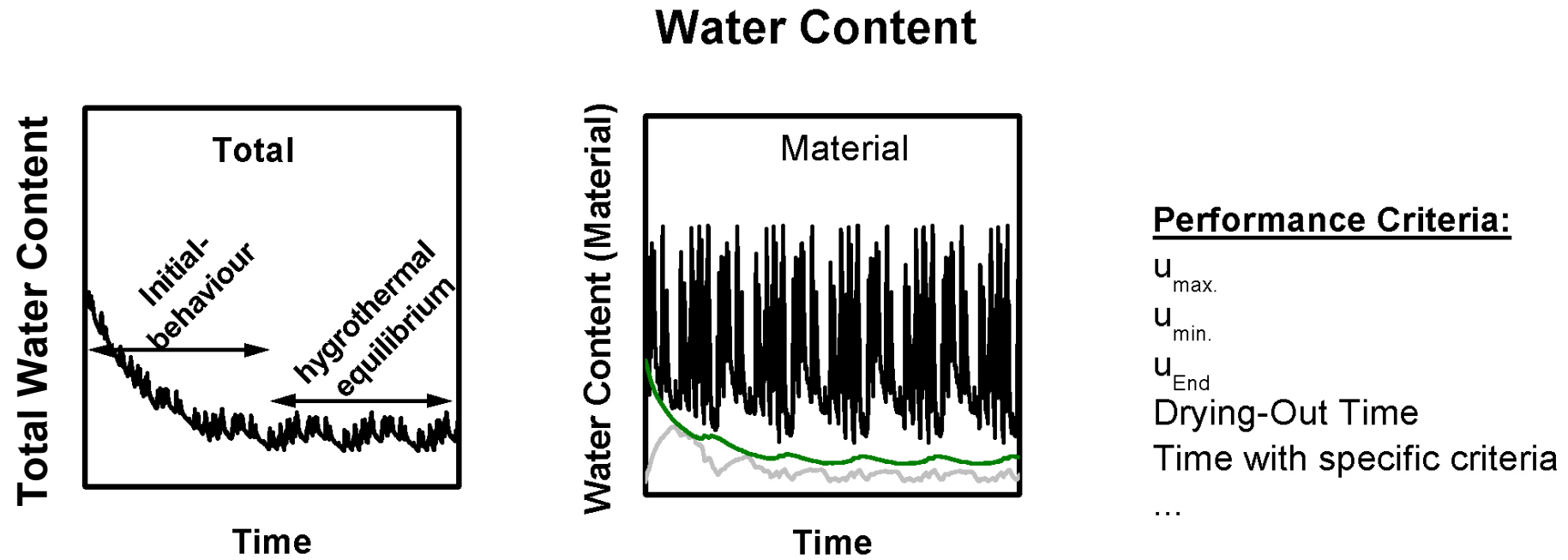
$u_{\min.}$

u_{End}

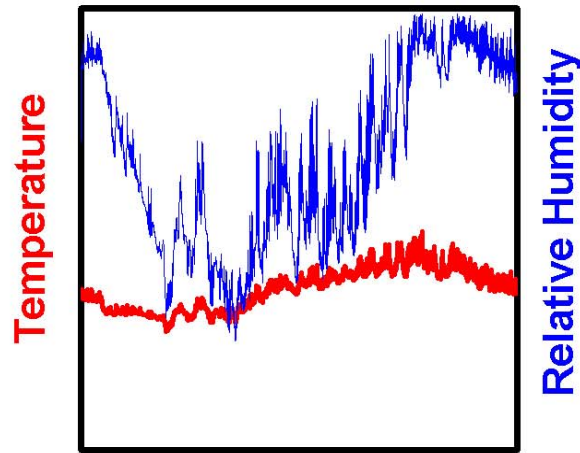
Drying-Out Time

Time with specific criteria

...



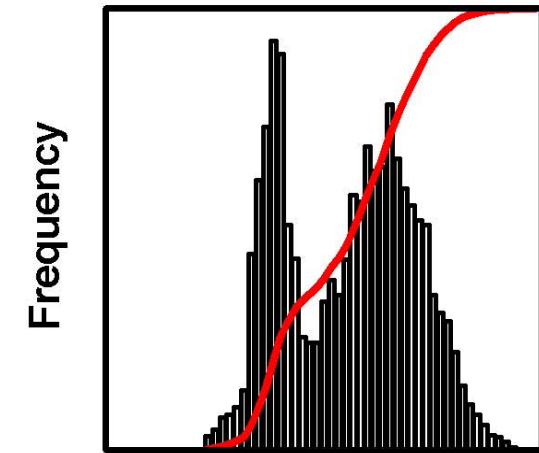
Hygrothermic Situation at Critical Points of the Construction



Time



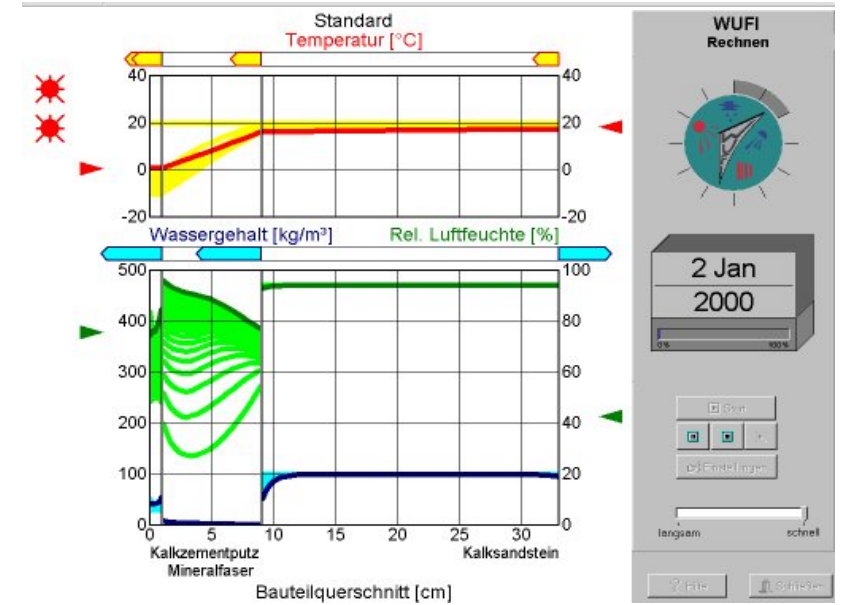
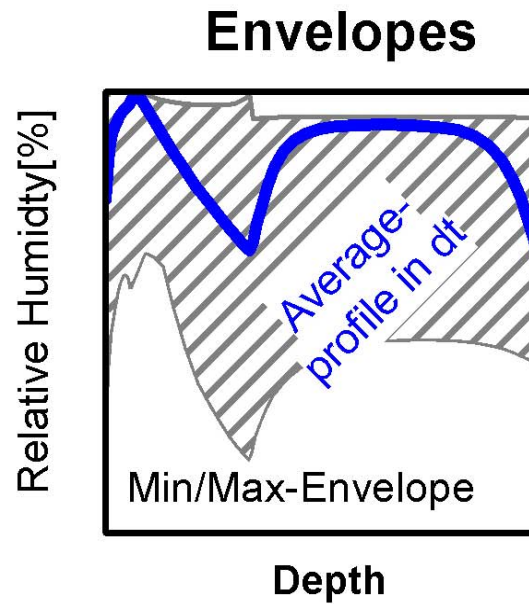
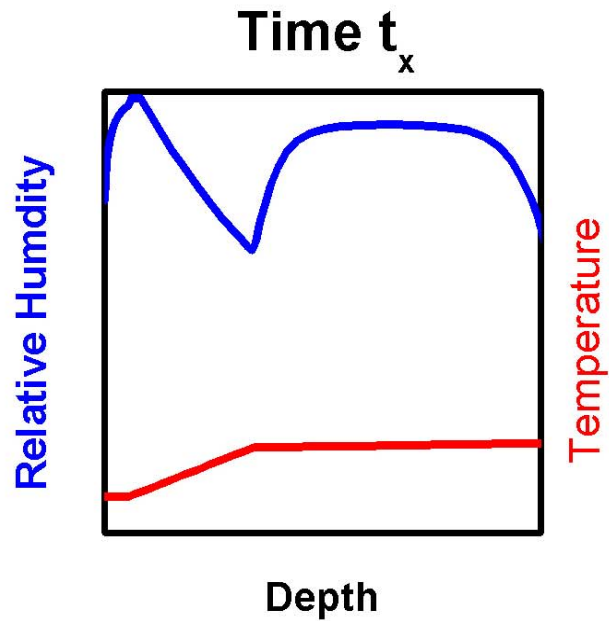
Temperature



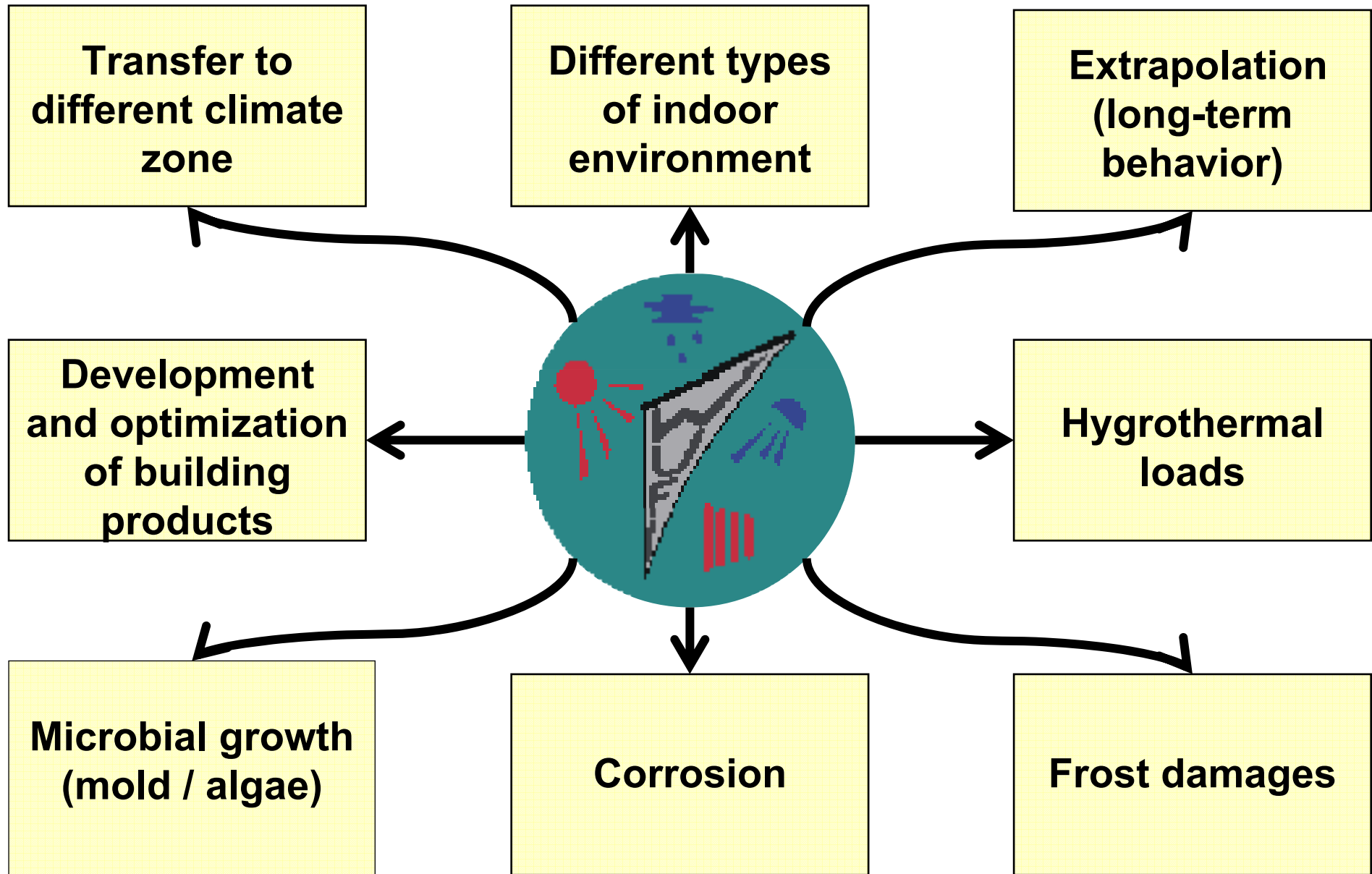
Temperature / RH

Building Envelope Design by Hygrothermal Simulations

Profiles



Building Envelope Design by Hygrothermal Simulations



Experimental Validation

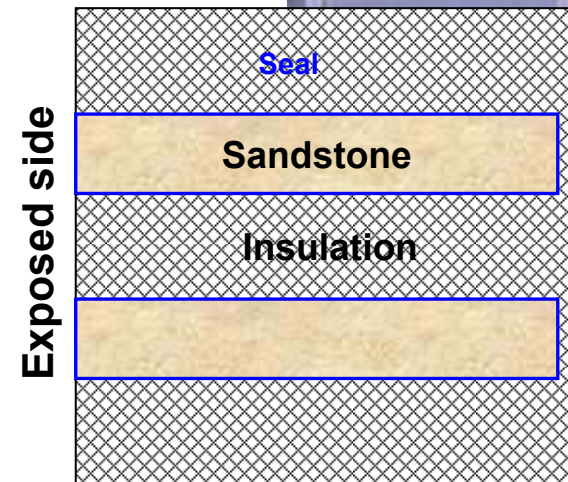
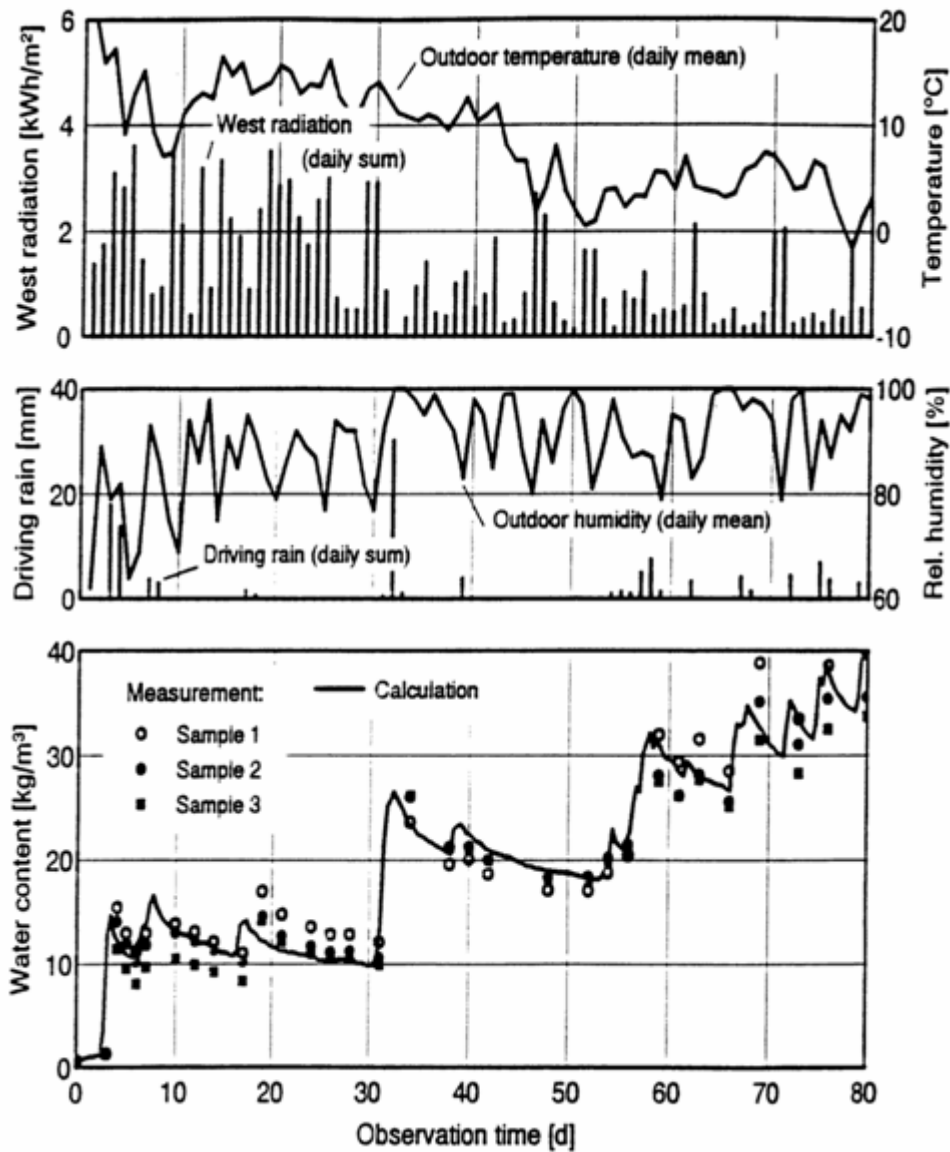
Prerequisites:

- ▶ well defined material parameters
(measured for the same material)
- ▶ hourly recording of boundary conditions
(natural climate)
- ▶ periodic or continuous readings of total
water content (weighing) and moisture
profiles (e.g. NMR- scanning)



IBP weather station

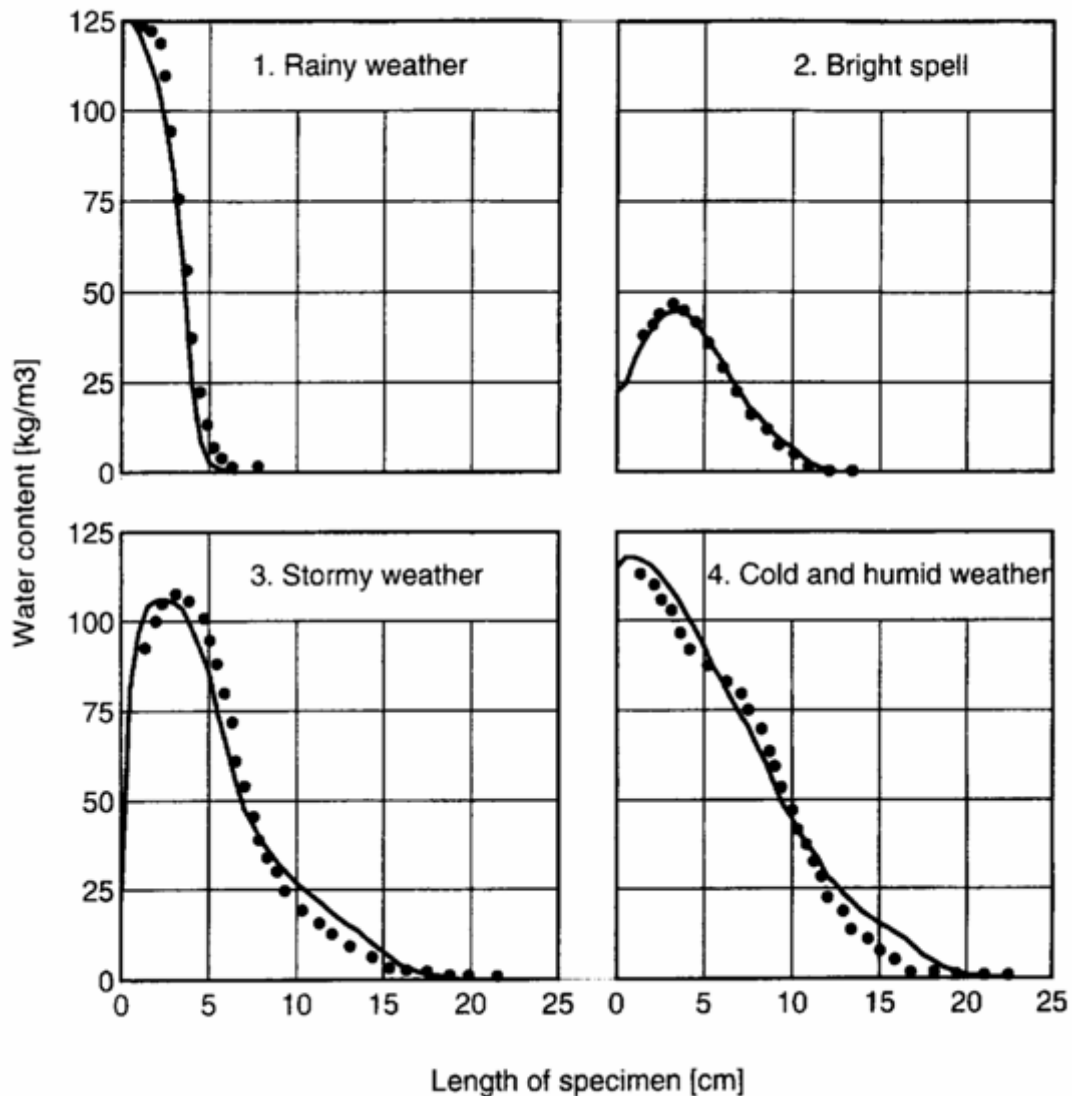
Experimental Validation



Comparison of total water content

Experimental Validation

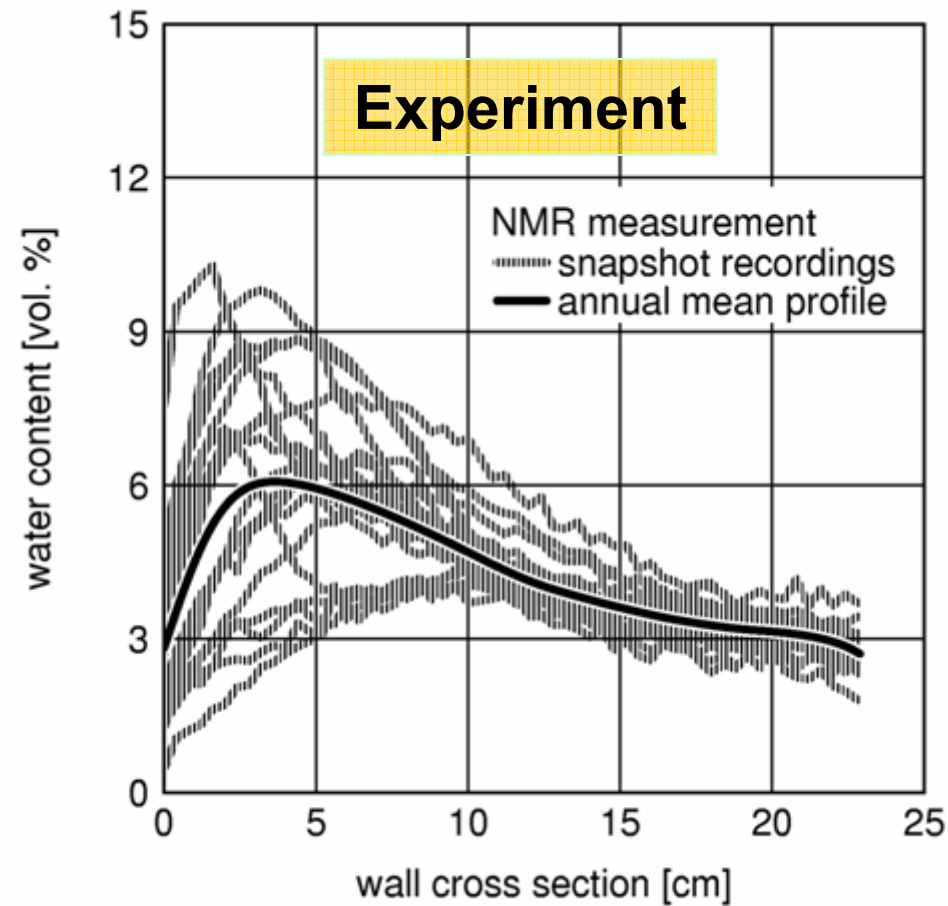
Sander sandstone



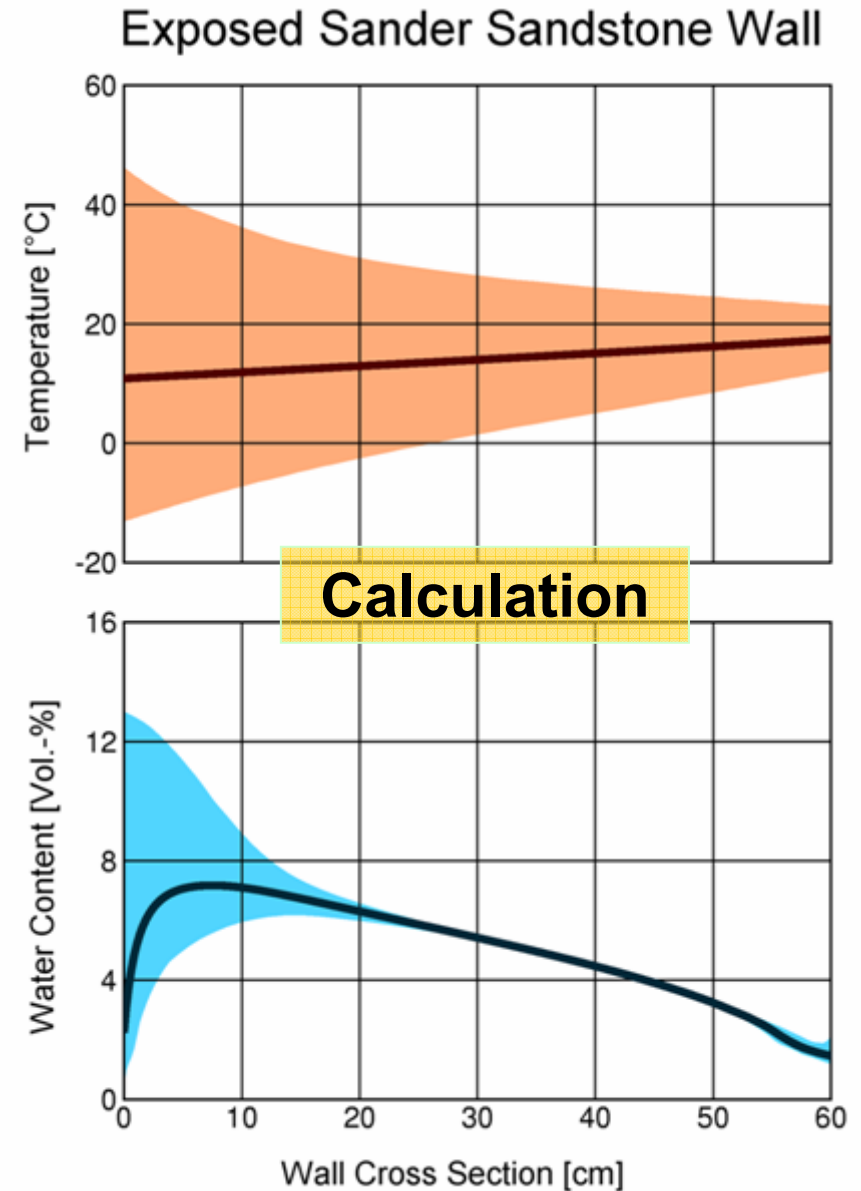
NMR-Scanner

Comparison of moisture distributions during a test period of 80 days

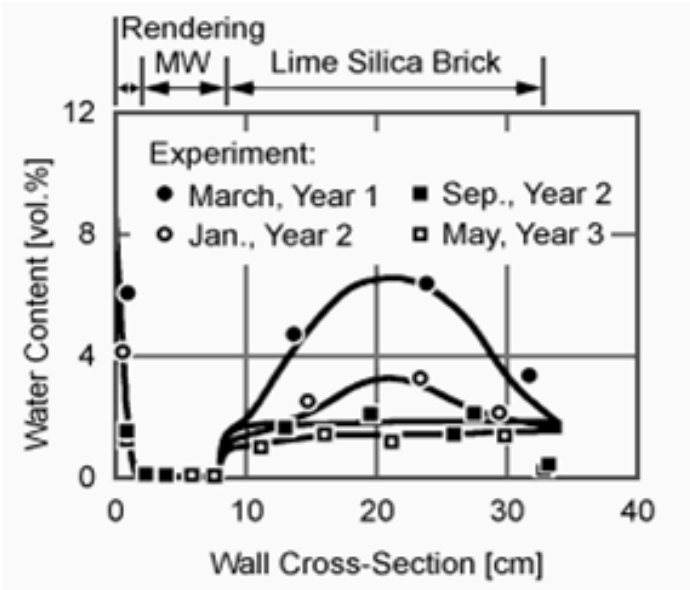
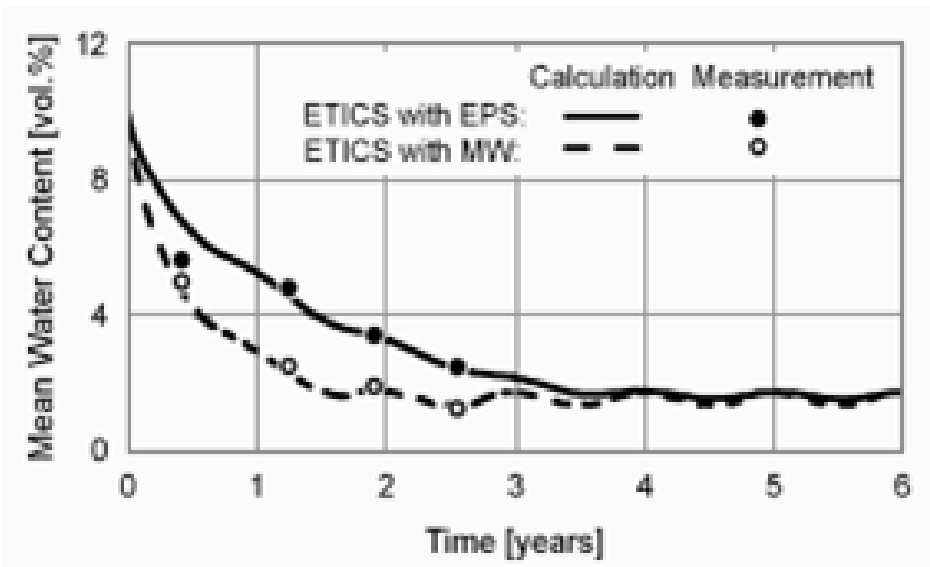
Experimental Validation



Comparison of long-term moisture profiles



Experimental Validation



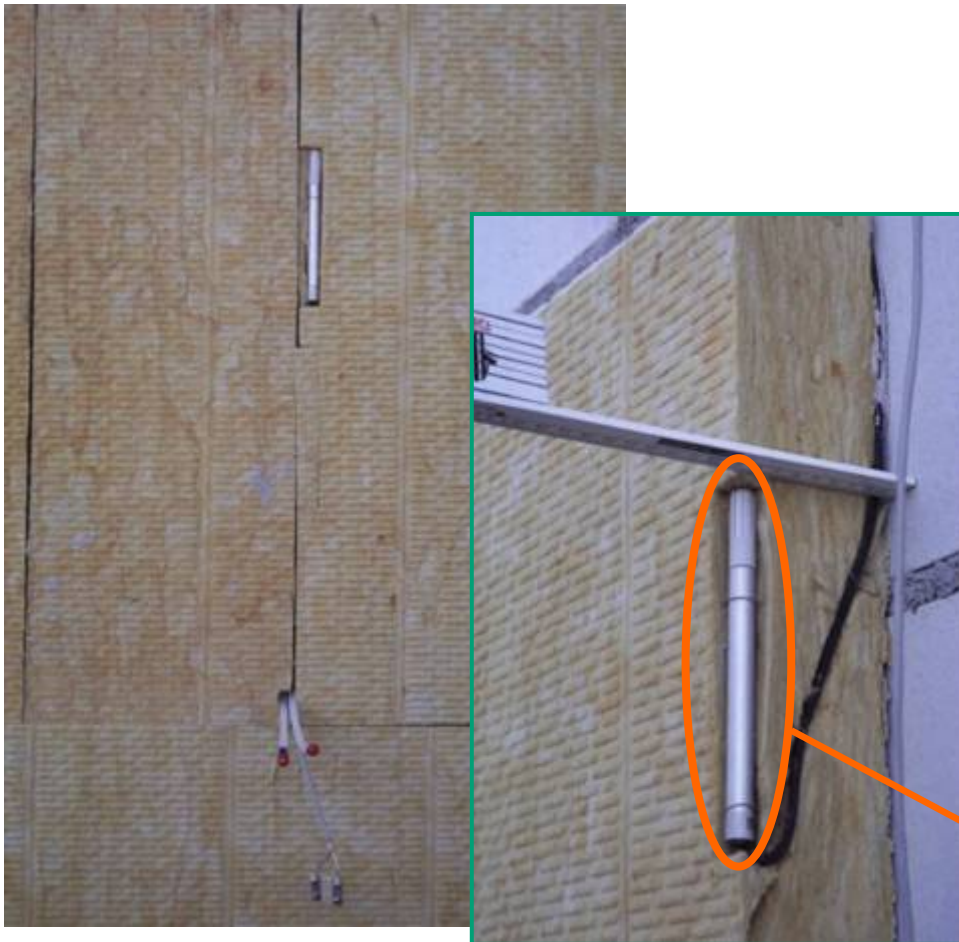
CSB wall
with exterior
insulation

Practice case: drying of construction moisture

Building Envelope Design by Hygrothermal Simulations

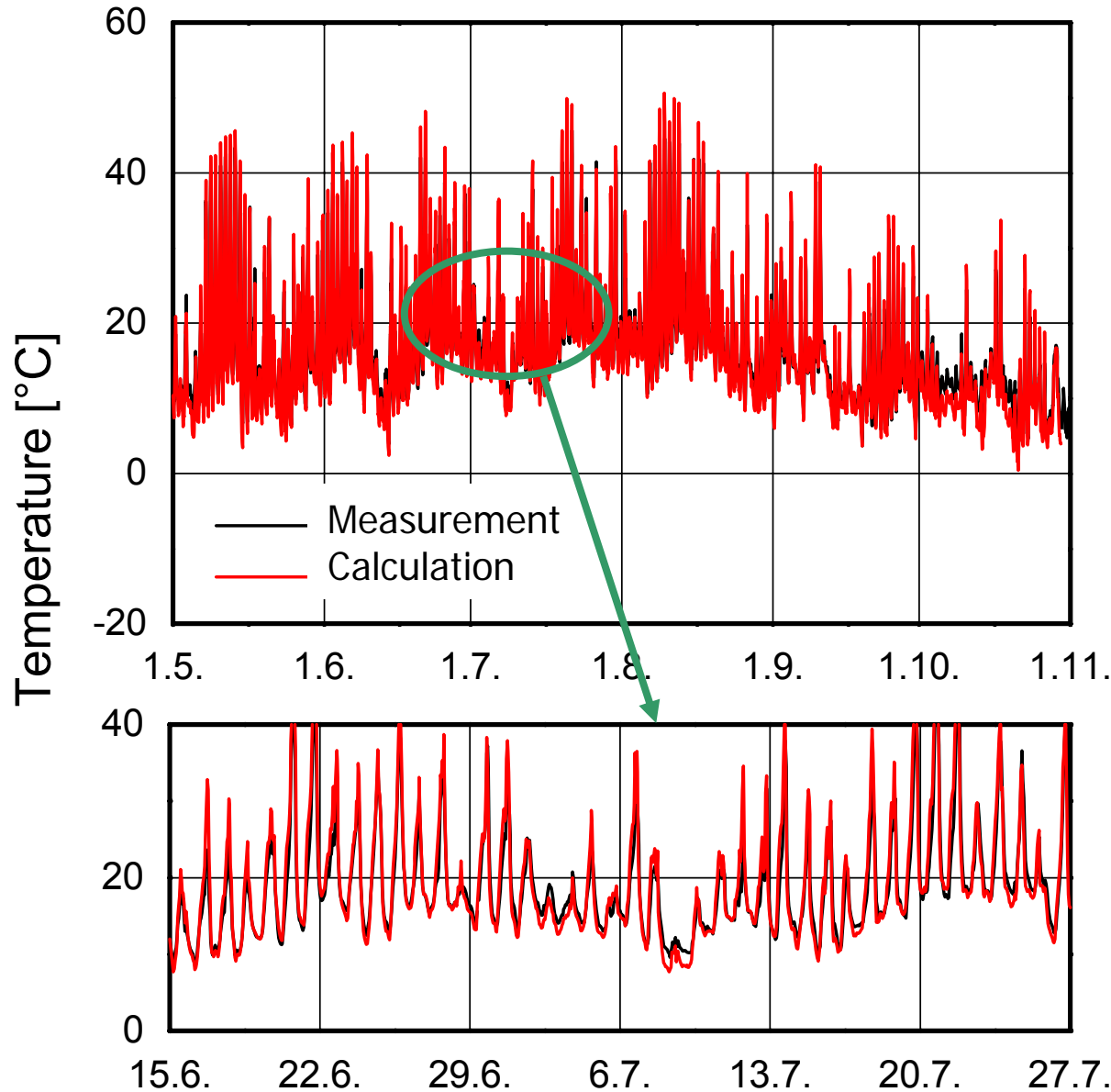
Experimental Validation

Comparison of temperature and RH fluctuations



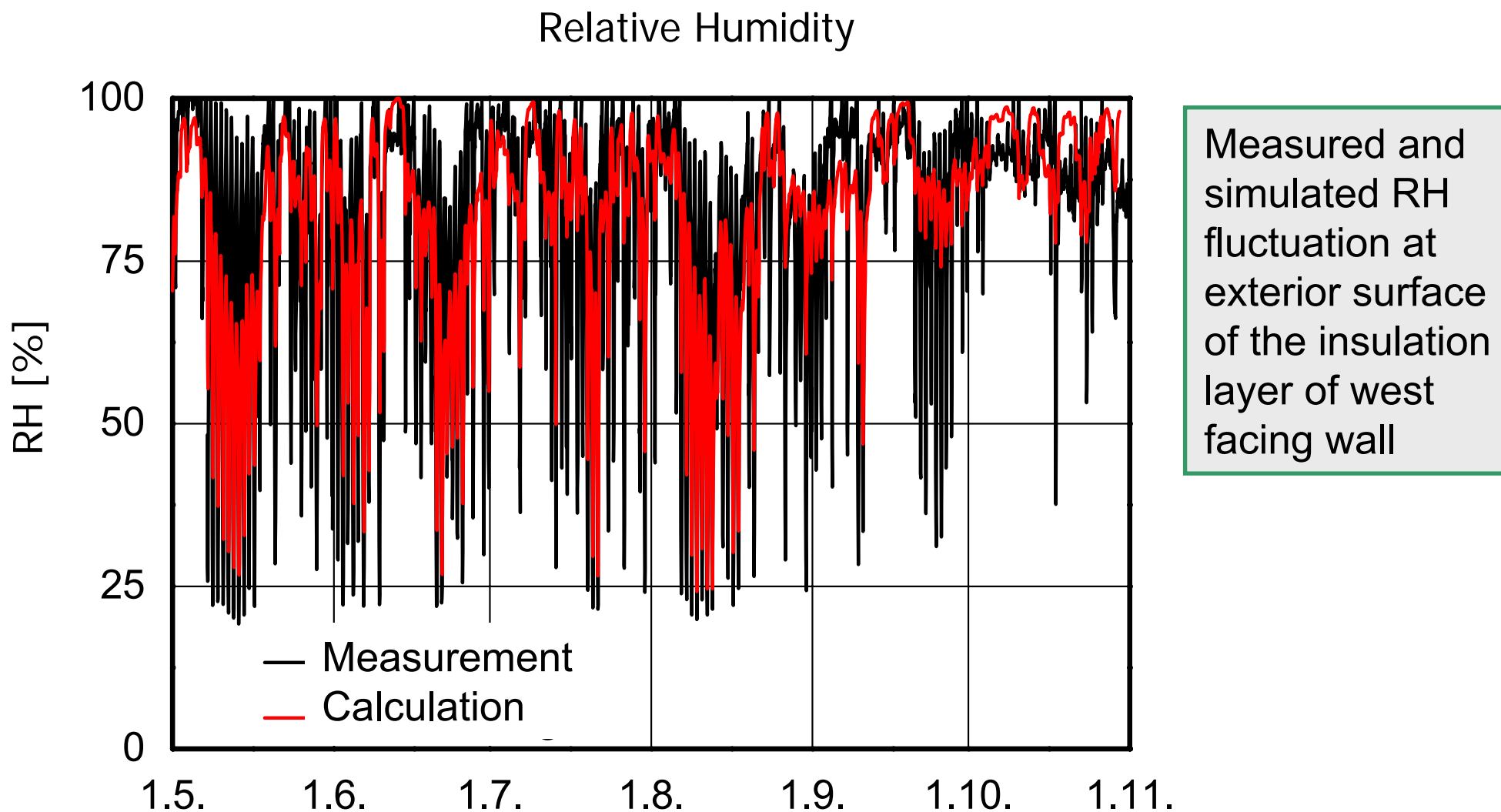
RH (capacitive sensor)
& temperature (PT100)

Experimental Validation



Measured and simulated temperature fluctuation at the exterior surface of the insulation layer of west facing wall

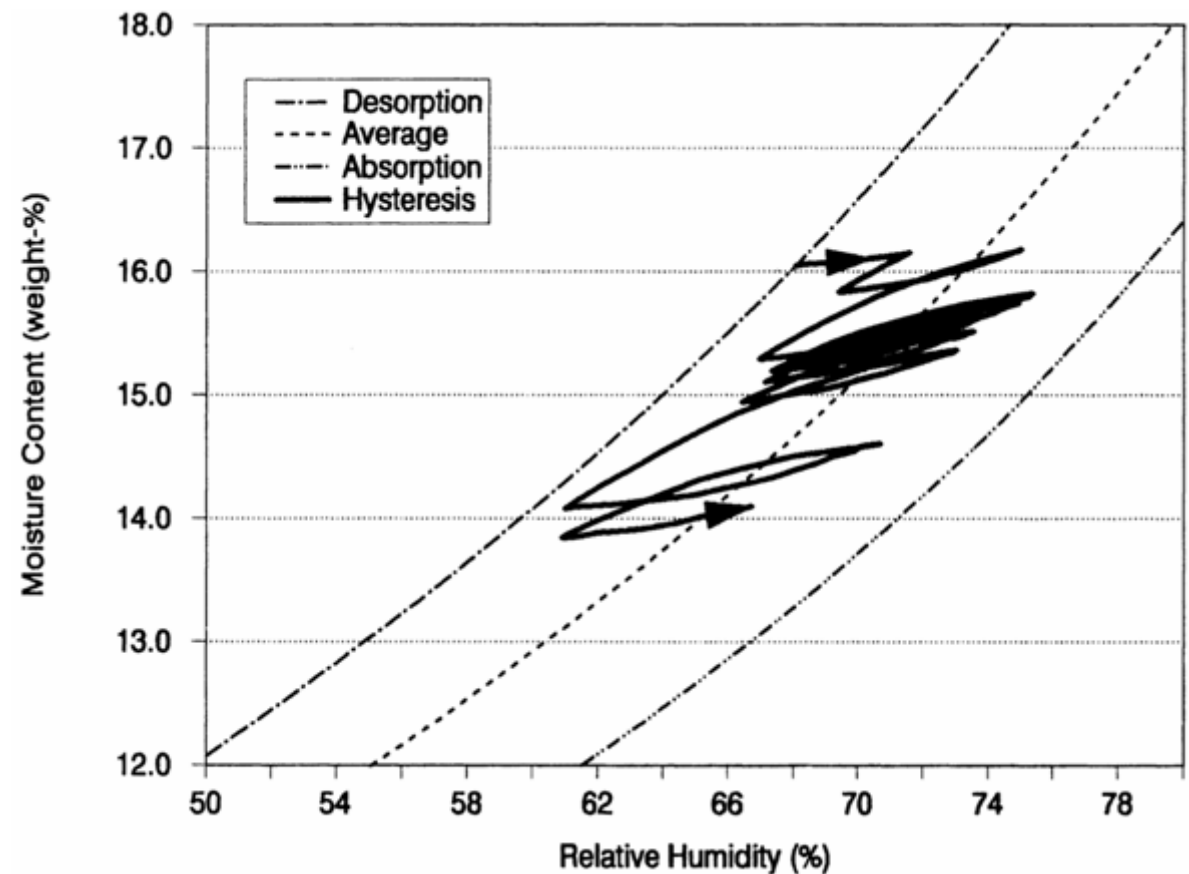
Experimental Validation



Experimental Validation

Local sorption equilibrium is not always achieved when fluctuations become very large:

- ▶ RH peaks dampened
- ▶ water content variations are still correct



Limitations of the Model

Every model has its shares of limitations. The user must be aware of what the model can do and cannot do.



Limitations of the Model

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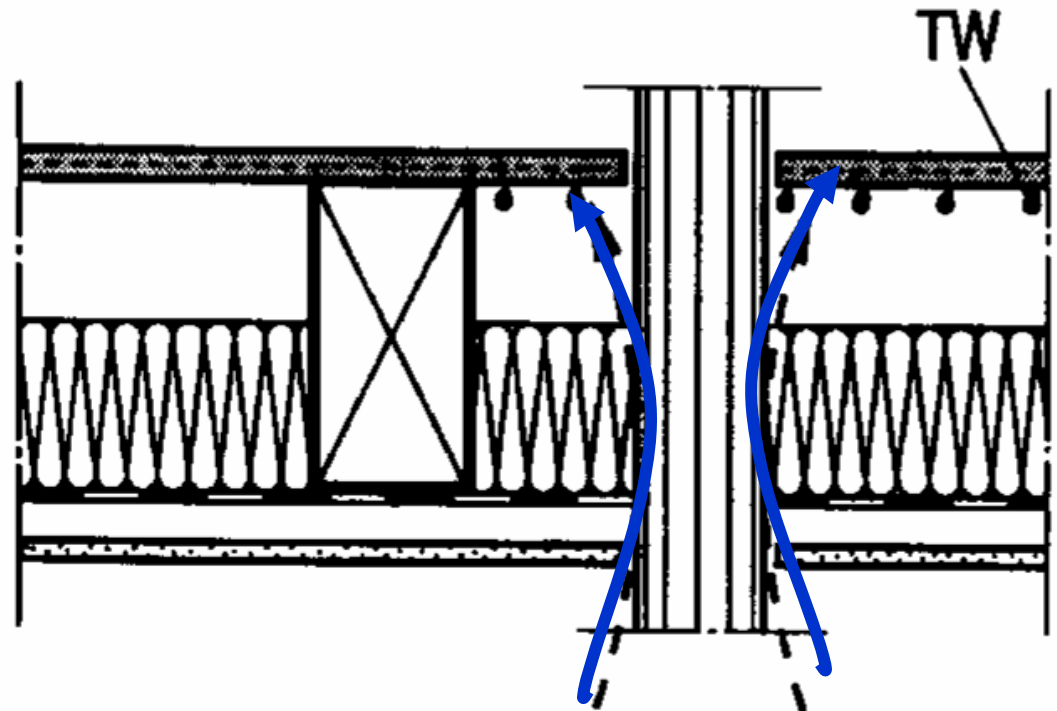
- ▶ More-dimensional structures



Limitations of the Model

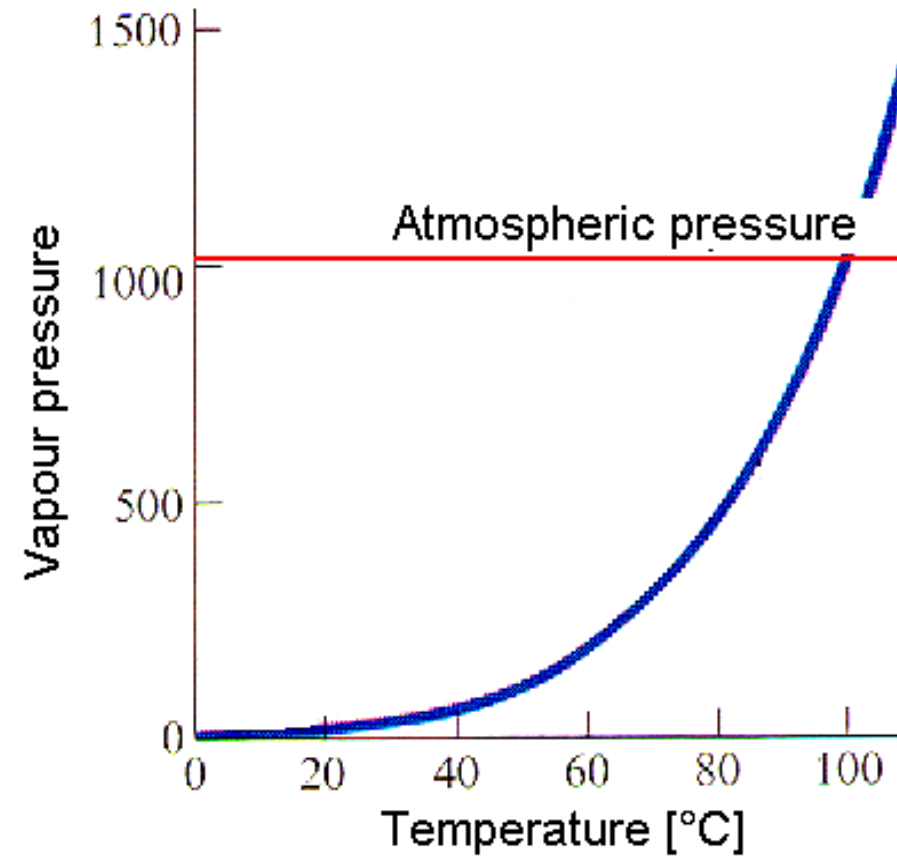
Every model has its shares of limitations. The user must be aware of what the model can do and cannot do.

- ▶ More-dimensional structures
- ▶ Special transport phenomena (e.g. convection)



Boundary Conditions

- ▶ temperatures $\gg 70$ °C (for example in case of fire)



Conclusions and Outlook

Benefits of hygrothermal envelope simulations:

- ▶ visualization of dynamic heat and moisture transfer process
 - diurnal cycles (e.g. summer condensation)
 - seasonal cycles (e.g. winter condensation)
 - wetting/drying cycles (e.g. rain/sunshine)
- ▶ distinction of relevant parameters (sensitivity analysis)
- ▶ extrapolation in time, transfer to different indoor or outdoor climate
- ▶ product adaptation, optimization and development

Hygrothermal simulations are fast and cost-effective, but:

- ▶ simulation results depend on reliability of input data
- ▶ user's expertise required !!!

Conclusions and Outlook

WUFI®-courses

Germany, Holzkirchen, Stuttgart, Hannover > 25x

Switzerland, Zürich (EMPA) 2x

Austria, Vienna (TU Wien) 2x

Finland, Helsinki (VTT)

Japan, Tokyo (Ochanomizu University)

Canada, Montreal (Université Concordia)

USA (ORNL) 10x (**Pennstate** University (PA), **Charleston** (SC), ASTM-Conference, **Boston** (MA), Boston Society of Architects **Seattle** (WA), Wash. State Univ., **Clemson** (SC), Clemson Univ., **San Diego** (CA), DOE workshop, **Chicago** (IL), DOE workshop, **Philadelphia** (PA), CT course, **Clearwater Beach** (FL), Buildings IX-Conference, **San Antonio**, (Tx) DOE workshop)

Cooperations to develop country specific WUFI®-versions

USA (ORNL = Oak Ridge National Laboratory)

Finland (VTT Building Technology)

France (CSTB Grenoble)

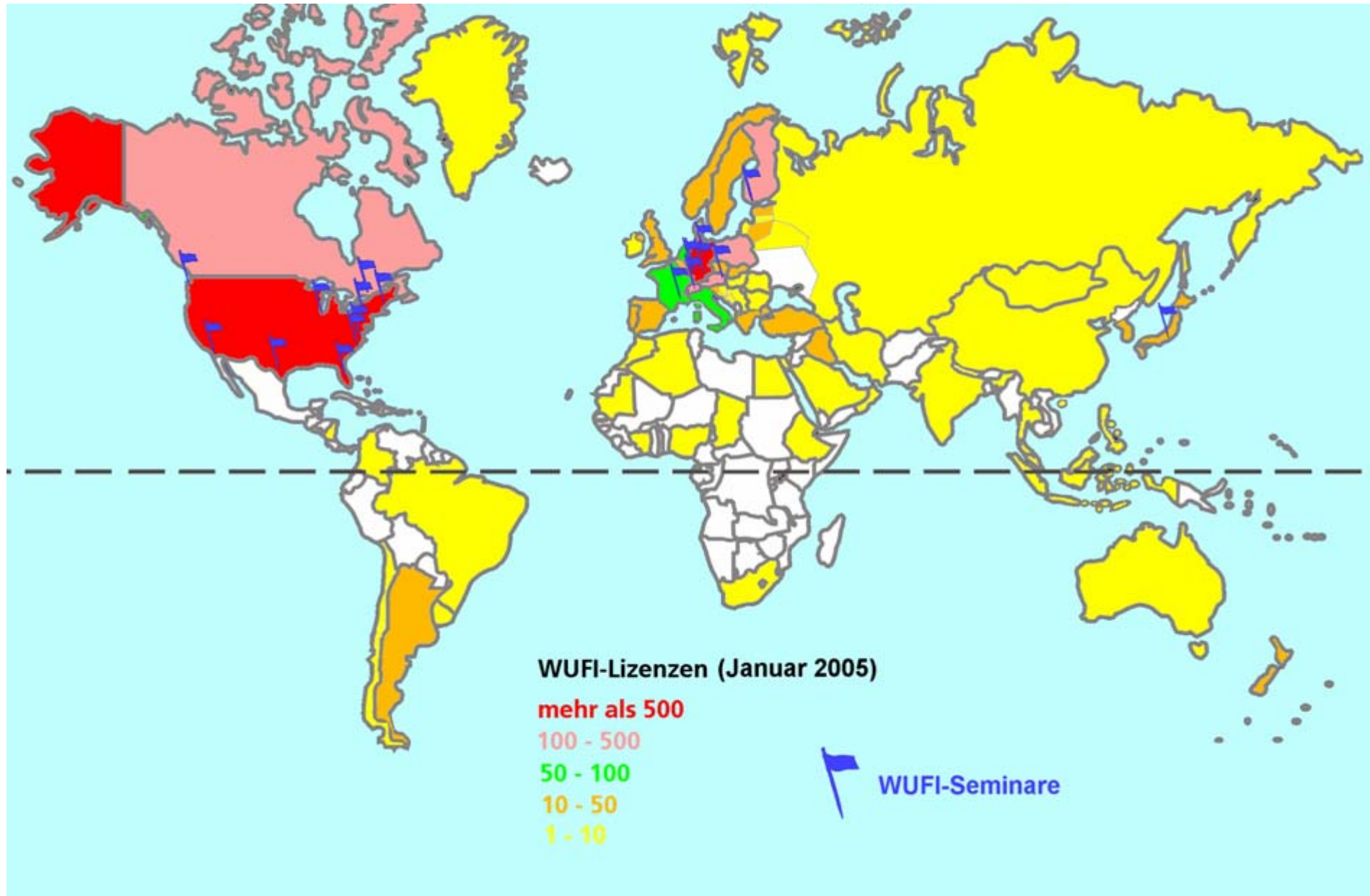
Poland (TU-Lodz)

Norway (NBI/NTNU)

Japan (Ochanomizu University)

Brazil (University Santa Catarina) *in preparation*

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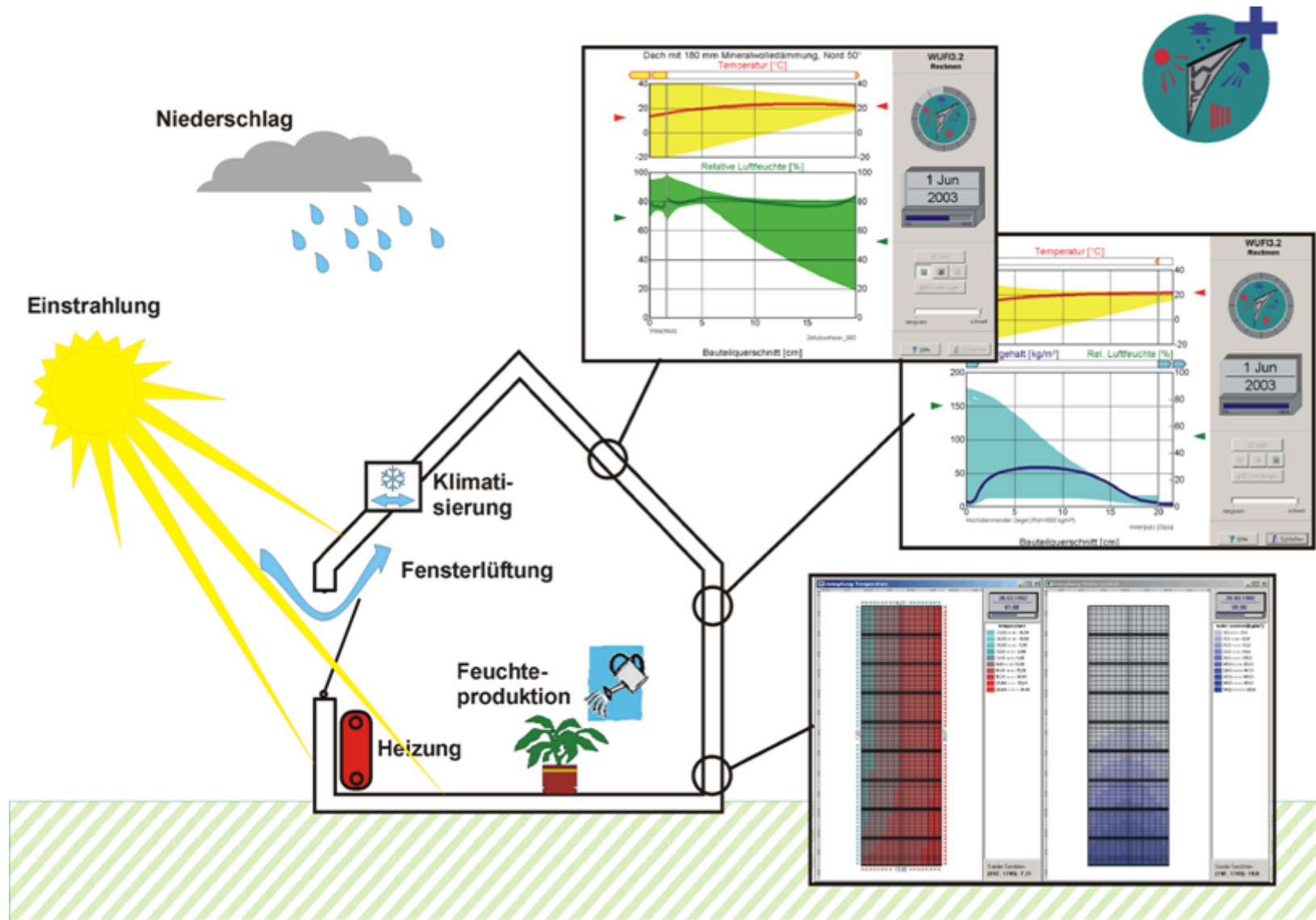
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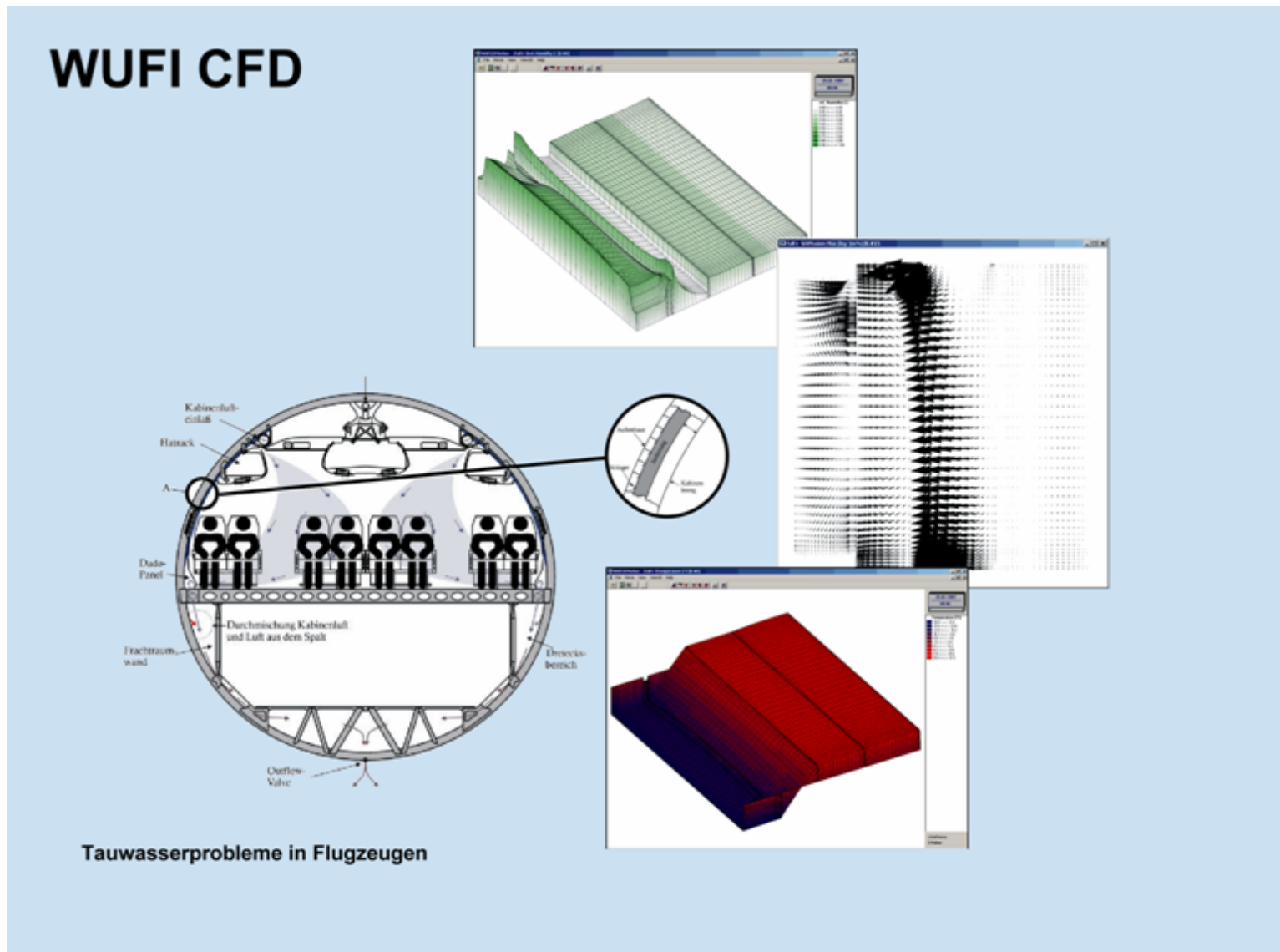
WUFI® R&D-team: Eitner, Pankratz, Kehrer, Zirkelbach, Künzel, Schmidt

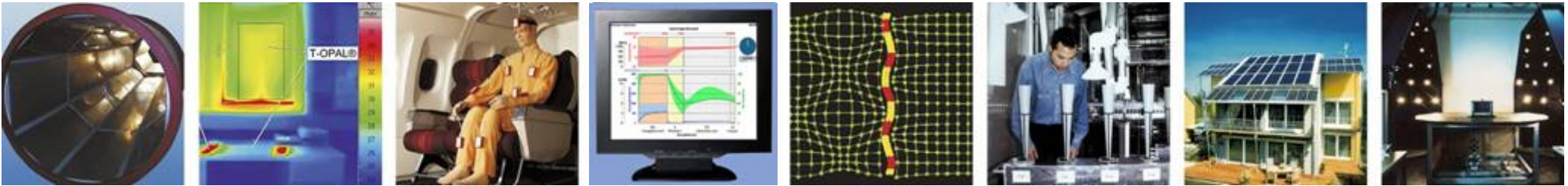
Building Envelope Design by Hygrothermal Simulations

Outlook: hygrothermal building simulation (WUFI®-Plus)



Outlook: CFD simulation with moisture transfer (WUFI®-CFD)





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